Sensing energy (heat) exchange at the nano-scale during H₂-uptake on Ti-functionalized graphene

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Outline



S. Veronesi Calorimetry at nano-scale

Motivation

A detailed knowledge of the energy exchange in the fast growing family of micro and nano-systems could allow to obtain valuable information about the chemistry and physics at the nano-scale. A calorimetric evaluation of tiny samples would represent a precious source of information in developing

- Sensors
- Catalyzers
- Molecules of pharmaceutical interest
- H-Storage devices

Even if performance is improving with time, commercial calorimeters are still far from the access to nano-scale samples.

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Calorimetry Setups Samples characterization

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commercial devices

Usually commercial devices require:

- sample mass in the mg range (usually 10 mg)
- limited energy sensitivity (~ mJ)

Sensitive thermometric techniques are able to measure milli-Kelvin temperature differences in devices at the nano-scale. But, they can operate only at low temperatures (below a few Kelvin).

What does it mean for Ti-Hydrogen system? If we want to detect 10 mg of H_2 on a MLG, considering US Department of Energy DOE prescriptions (5.5 wt.%) and the specific surface area of graphene ($\sim 2600 m^2/g$) we will need $\sim 450 m^2$ of MLG.

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Our original calorimetric technique has been tested on a Ti-functionalized MLG sample, which is a system well investigated. Overall sample mass is **10 ng**, 6 order of magnitude lower than commercial device request.

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Sample & holder







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Thermometer working principle

All experiments are performed in Ultra-High Vacuum (UHV) environment (base pressure $\sim 10^{-10}$ mbar). Temperature is measured via the gold film resistance, following the linear relation:

 $R(T) = R_0 [1 + \alpha (T - T_0)]$ where R_0 is the resistance at the reference temperature T_0 (room temperature in our case) and α is the resistance temperature coefficient.



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STM analysis



Figure: (a) STM image of the Au layer. Image parameters: V=1.0 V, I=1.0 nA, average RMS roughness: (0.8 ± 0.2) nm. (b) STM image of the MLG transferred on the Au layer. Image parameters: V=0.6 V, I=0.5 nA, average RMS roughness: (1.7 ± 0.5) nm. The inset shows a cross-sectional plot of a wrinkle taken along the blue line in the STM image. (c) STM image of 12.4 ML Ti evaporated on MLG. Image parameters: V=0.2 V, I=0.09 nA, average RMS roughness: (2.0 ± 0.5) nm. All images 500 × 500 nm².

Hydrogen uptake Enthalpy of process evaluatio

Outline



Motivation Experimental setup Experimental Results

Conclusions and Outlook

H<mark>ydrogen uptake</mark> Enthalpy of process evaluatio

Calorimetry during hydrogenation



(a) Ti deposition (for 539 s, 12.4 ML of Ti) on MLG. (b)Exposure of the Ti film to D₂(red line: exponential fit of the thermalization background). (c) Thermalization background subtracted. A $\Delta T = 0.065$ K is clearly detected. (d) TDS spectrum of Ti-MLG (Red line: smoothing).

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TDS analysis



Hydrogen uptake Enthalpy of process evaluation

TDS analysis



$$p V = F S = n R T$$

 $C \sim 200 L/c$

$$n(D_2) \rightarrow 1.71 \cdot 10^{-10} \text{ mol}$$

$$H_r = n N_A E_b = (21.8 \pm 1.3) \,\mu\text{J}$$

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Thermal model

We can describe the system with a simple thermal model in which the thermometer is heated by the absorption of a thermal power $P(t) = \delta H_r / \delta t$ while at the same time it releases energy by heat losses towards the substrate. These two contributions are related by the following equation:

$$\delta H_r / \delta t = C \cdot \delta \Delta T(t) / \delta t + \lambda \cdot \Delta T(t)$$

The sensor heat capacity C and the thermal exchange coefficient λ must be evaluated.

M. Cassettari, F. Papucci, G. Salvetti, E. Tombari, S. Veronesi, G. Johari, "Simultaneous measurements of enthalpy and heat capacity of a thermosetting polymer during the curing process" Review of Scientific Instruments 1993, **64**, 1076-1080

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Heat capacity and losses evaluation

$$\Delta T(t) = \Delta T(0) + A_1 e^{-t/\tau_1} + A_2 e^{-t/\tau_2} + A_3 e^{-t/\tau_3}$$





From the decay curve analysis and comsol simulation can be figure out

- the total heat capacity $C = (15.0 \pm 0.2) \cdot 10^{-6} \text{ J/K}$ with $C = C_{Au} + C_{Ti} + C_{SiO_2}$.
- The heat exchange coefficient λ as $\lambda = C/\tau_1 = (5.1 \pm 1.1) \cdot 10^{-6}$ W/K.

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Enthalpy calculation



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Next generation of thermometer based on Mica substrate



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Next generation of thermometer

An issue to solve is relative to surface roughness. Atomically speaking Gold thermometer has a rough surface which do not allow atomic resolution with STM. Mica allows surface reconstruction of Gold, solving this problem.







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Next generation of thermometer

Moreover, the new sensor substrate (Mica) allows a better performance in terms of sensitivity.



Conclusions and Outlook

First direct measurement of enthalpy release during Hydrogen adsorption process

- resistance readout sensitivity $\sim 0.03 m\Omega$
- temperature variation sensitivity 10mK
- H_2 detected during adsorption ~ 0.2*ng* or $(1.71 \pm 0.01) \cdot 10^{-10}$ moles
- advantages:
 - calorimetric evaluation is direct and do not need H₂ desorption, while TDS need the desorption of the loaded H₂
 - in presence of a desorption barrier the calorimetric evaluation is not affected while TDS would include it
- Simultaneous investigation of energy transfer mechanisms and STM analysis on the same physical support

People



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thanks

Thank you for your attention

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Raman Spectroscopy





Figure: (a) Raman intensity ratio map: each pixel gives the ratio between the intensity of the 2D peak vs the *G* peak. (b) Raman map showing the FWHM (in cm⁻¹) of the 2*D* peak.

COMSOL simulation



Figure: (a) Temperature distribution at t = 1 ns when the temperature jump of 2 K has just been applied to the topmost layer of the stack. All other parts of the stack are still at 303 K. (b) Temperature distribution at $t = 0.1 \ \mu s$.

Simulation mesh



Figure: (a) Evaluation mesh (free Triangular with a Normal Size) utilized in the COMSOL simulation. (b) Zoom–in of the top part of the sample.

Thermometer + MLG + Ti characterization



Ramp	α_f (K ⁻¹)
1	$(1.57\pm0.01)\cdot10^{-3}$
2	$(1.56 \pm 0.01) \cdot 10^{-3}$
3	$(1.58 \pm 0.02) \cdot 10^{-3}$
4	$(1.64 \pm 0.02) \cdot 10^{-3}$
5	$(1.63 \pm 0.02) \cdot 10^{-3}$
6	$(1.72\pm0.02)\cdot10^{-3}$

Table: Temperature coefficient of resistance (α_f) for each of the heating ramps presented in Figure. The average value is $\alpha_f = (1.62 \pm 0.05) \cdot 10^{-3} \text{ K}^{-1}$.

Figure: Resistance variation ($\Delta R = R(T) - R_0$) vs. temperature for six different heating experiments on the same Au+Ti–MLG sensor.

Calorimetry

The enthalpy variation consists in the change in internal energy ΔU plus the work L needed to change the system's volume V. Working at constant pressure allows a simplified relation between Enthalpy variation ΔH and heat exchanged δQ :

$$\Delta H = \Delta U + L = C_{p} \cdot \Delta T + V \cdot \Delta P = \delta Q + V \cdot \Delta P$$

In case of exothermic or endothermic reactions (with time-independent C_p):

$$\frac{\delta H_r}{\delta t} = C_p \cdot \frac{\delta \Delta T}{\delta t} + \lambda \cdot \Delta t$$

where $\lambda \cdot \Delta t$ represent losses toward the substrate