Bridging heat exchange and surface physics investigations on samples at the nano-scale

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Outline

- Motivation
 - Nano-scale Calorimetry
- 2 Experimental setup
 - Setups
- 3 Experimental Results
 - Hydrogen uptake
 - Evaluation of process enthalpy
- Thermometer 2.0 Gold on Mica
- Conclusions and Outlook

Motivation

A detailed knowledge of the energy exchange in the fast growing family of microand nano-systems could allow to obtain valuable information about the chemistry and physics at the nano-scale. A calorimetric evaluation of tiny samples would represent a precious source of information in developing

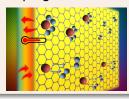
- Sensors
- Catalyzers
- Molecules of pharmaceutical interest
- H-Storage model systems

Even if performance is improving with time, commercial calorimeters are still far from the access to nano-scale samples.

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samples and signals

In performing calorimetry on nano-systems in an UHV environment, two aspects must be taken into account:

- sample mass
- thermal signal characteristics

Typically a sample based on a 2D material spans at most over a few square mm area, that means a mass in the ng range.

A chemical reaction occurring in an UHV environment between a functionalized surface and a gas atom/molecule runs slowly.

At a gas supply pressure of 10^{-7} - 10^{-8} mbar, the time necessary to have a monolayer on the surface is 10-100 s.

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commercial devices

Usually commercial devices require:

- sample mass in the mg range (usually 10 mg)
- Iimited energy sensitivity (∼ mJ)

Sensitive thermometric techniques are able to measure milli-Kelvin temperature differences in devices at the nano-scale. But, they can operate only at low temperatures (below a few Kelvin).

What does this mean for the Ti-Hydrogen system? If we want to detect 10 mg of H_2 on a MLG, considering the US Department of Energy DOE prescriptions (5.5 wt.%) and the specific surface area of graphene (\sim 2600 m²/g) we will need \sim 450 m² of MLG.

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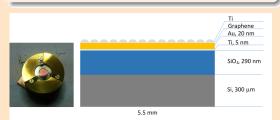
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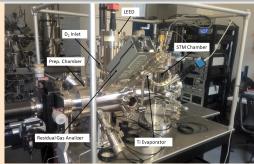
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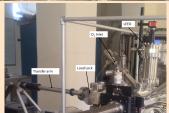
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Sample & holder

Our original calorimetric technique has been tested on a Ti-functionalized monolayer graphene (MLG) sample, which is a system well investigated. Overall sample mass is 10 ng, 6 orders of magnitude lower than commercial devices request.







Thermometer and thermal model

All experiments are performed in Ultra-High Vacuum (UHV) environment (base pressure $\sim 10^{-10} mbar$). Temperature is measured via the gold film resistance, following the linear relation:

$$extbf{\textit{R}}(extbf{\textit{T}}) = extbf{\textit{R}}_0 \left[1 + lpha \left(extbf{\textit{T}} - extbf{\textit{T}}_0
ight)
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where R_0 is the resistance at the reference temperature T_0 (room temperature in our case) and α is the resistance temperature coefficient.

We can describe the system with a simple thermal model in which the thermometer is heated by the absorption of a thermal power $P(t) = \delta H_r/\delta t$, where H_r is the released enthalpy, while at the same time it releases energy by heat losses towards the substrate These two contributions are related by the following equation:

$$\delta H_r/\delta t = C \cdot \delta \Delta T(t)/\delta t + \lambda \cdot \Delta T(t)$$

The sensor heat capacity C and the thermal exchange coefficient λ must be evaluated.

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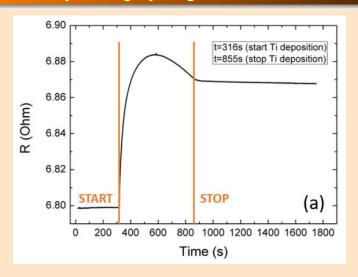
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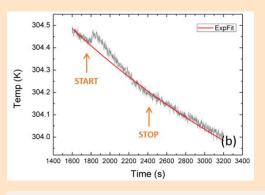
Calorimetry during hydrogenation: Ti-functionalization

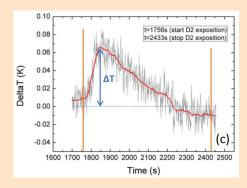


(a) Ti deposition: thermometer heating during the Ti deposition (for 539 s, 12.4 ML of Ti) on MLG.



Calorimetry during hydrogenation: heat release

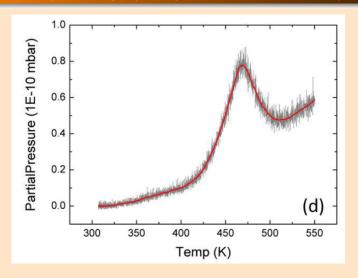




- (b) Exposure of the Ti film to D₂ (red line: exponential fit of the thermalization background).
- (c) Thermalization background subtracted. A $\Delta T = 0.065$ K is clearly detected.



Calorimetry during hydrogenation: TDS analysis



(d) TDS spectrum of Ti–MLG (Red line: smoothing).

Outline

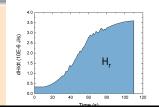
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Enthalpy calculation

Calorimetry

$$\delta H_r/\delta t = C \cdot \delta \Delta T(t)/\delta t + \lambda \cdot \Delta T(t)$$

- Total heat capacity $C = (15.0 \pm 0.2) \cdot 10^{-6} \text{ J/K}$ with $C = C_{AU} + C_{Ti} + C_{SiO_2}$.
- Heat exchange coefficient λ $\lambda = C/\tau_1 = (5.1 \pm 1.1) \cdot 10^{-6}$ W/K.
- Enthalpy release $H_r = (23.4 \pm 4.7) \mu J$



TDS analysis

- Binding energy $E_d = (1.32 \pm 0.07)eV/Molecule$
- Amount of adsorbed D_2 $n(D_2) = 1.7 \times 10^{-10}$ moles
- Enthalpy release $H_r = (21.8 \pm 1.3) \mu J$



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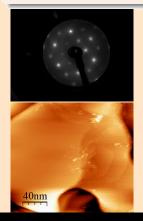
Next generation of thermometer

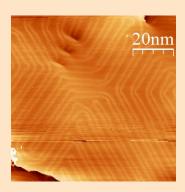
An issue to solve is relative to surface roughness. Atomically speaking Gold on SiO_2 thermometer has a rough surface which does not allow atomic resolution with STM. Mica allows Gold epitaxial recrystallization and surface reconstruction, solving this problem.

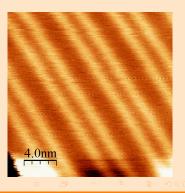
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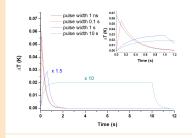


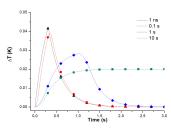
thermometer simulation

main contribution to thermalization time:

- Gold film $t_{Au} = d^2/\alpha \sim 4x10^{-12}s$
- Interface gold-mica
- Mica substrate $t_{Mica} = d^2/\alpha \sim 0.3s$
- Interface mica-holder

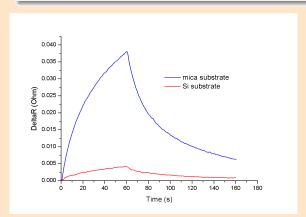
Simulation	Heating duration	Integration time	ΔE/E
	s	ms	
1	10^{-9}	300	0.04
2	10^{-1}	300	0.053
3	1	300	0.007
4	10	300	0.005





Next generation of thermometer

Moreover, the new sensor substrate (Mica) allows a better performance in terms of sensitivity.





Conclusions and Outlook

First direct measurement of enthalpy release during Hydrogen adsorption process

- resistance readout sensitivity $\sim 0.03 m\Omega$
- temperature variation sensitivity 10*mK* (Si substrate), 4*mK* (Mica substrate)
- H_2 detected during adsorption $\sim 0.2ng$ or $(1.71 \pm 0.01) \cdot 10^{-10}$ moles
- advantages:
 - calorimetric evaluation is direct and does not need H₂ desorption, while TDS need the desorption of the loaded H₂
 - in presence of a desorption barrier the calorimetric evaluation is not affected while TDS would include it
- Simultaneous investigation of energy transfer mechanisms and STM analysis on the same physical support



Experimental setup
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People





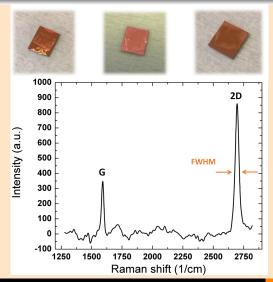




thanks

Thank you for your attention

Raman Spectroscopy



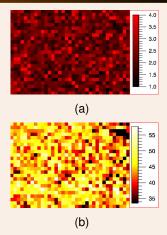


Figure: (a) Raman intensity ratio map: each pixel gives the ratio between the intensity of the 2D peak vs the G peak. (b) Raman map showing the FWHM (in cm⁻¹) of the 2D peak.

COMSOL simulation

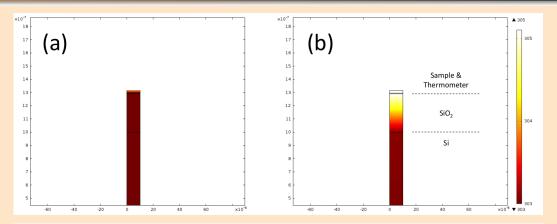
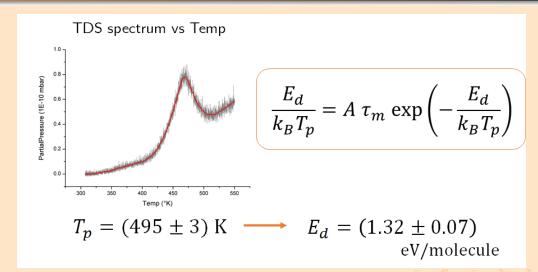


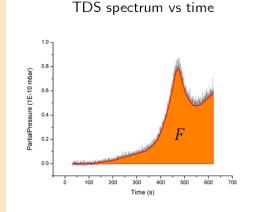
Figure: (a) Temperature distribution at t = 1 ns when the temperature jump of 2 K has just been applied to the topmost layer of the stack. All other parts of the stack are still at 303 K. (b) Temperature distribution at $t = 0.1 \mu s$.

TDS analysis



TDS analysis





$$pV = FS = nRT$$

$$S \approx 300 \, \text{L/s}$$



$$n(D_2) \to 1.71 \cdot 10^{-10} \text{ mol}$$

$$H_r = n N_A E_b = (21.8 \pm 1.3) \,\mu\text{J}$$

Heat capacity and losses evaluation

$$\Delta T(t) = \Delta T(0) + A_1 e^{-t/\tau_1} + A_2 e^{-t/\tau_2} + A_3 e^{-t/\tau_3}$$

$$\succ \tau_1 = (2.9 \pm 0.2) \text{ s}$$

$$\succ \tau_2 = (47 \pm 2) \text{ s}$$

$$\succ \tau_3 = (475 \pm 5) \text{ s}$$

From the decay curve analysis and comsol simulation can be figure out

- the total heat capacity $C = (15.0 \pm 0.2) \cdot 10^{-6} \text{ J/K}.$
- The heat exchange coefficient λ as $\lambda = C/\tau_1 = (5.1 \pm 1.1) \cdot 10^{-6}$ W/K.

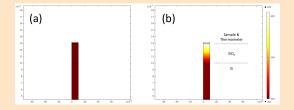


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Simulation mesh

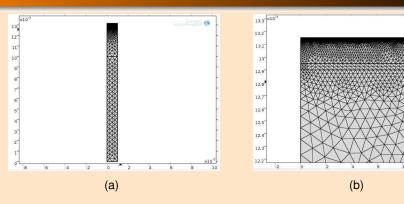


Figure: (a) Evaluation mesh (free Triangular with a Normal Size) utilized in the COMSOL simulation. (b) Zoom–in of the top part of the sample.

Thermometer + MLG + Ti characterization

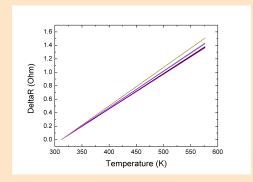


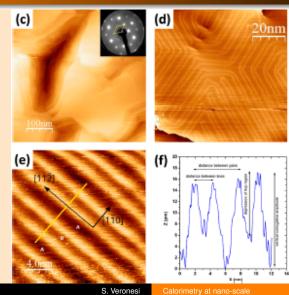
Figure: Resistance variation ($\Delta R = R(T) - R_0$) vs. temperature for six different heating experiments on the same Au+Ti–MLG sensor.

Ramp	α_f (K ⁻¹)	
1	$(1.57 \pm 0.01) \cdot 10^{-3}$	
2	$(1.56 \pm 0.01) \cdot 10^{-3}$	
3	$(1.58 \pm 0.02) \cdot 10^{-3}$	
4	$(1.64 \pm 0.02) \cdot 10^{-3}$	
5	$(1.63 \pm 0.02) \cdot 10^{-3}$	
6	$(1.72 \pm 0.02) \cdot 10^{-3}$	
	1 2 3 4 5	

Table: Temperature coefficient of resistance (α_f) for each of the heating ramps presented in Figure. The average value is $\alpha_f = (1.62 \pm 0.05) \cdot 10^{-3} \text{ K}^{-1}$.

Conclusions and Outlook

Profile



Calorimetry

The enthalpy variation consists in the change in internal energy ΔU plus the work L needed to change the system's volume V. Working at constant pressure allows a simplified relation between Enthalpy variation ΔH and heat exchanged δQ :

$$\Delta H = \Delta U + L = C_p \cdot \Delta T + V \cdot \Delta P = \delta Q + V \cdot \Delta P$$

In case of exothermic or endothermic reactions (with time-independent C_p):

$$\frac{\delta H_r}{\delta t} = C_p \cdot \frac{\delta \Delta T}{\delta t} + \lambda \cdot \Delta t$$

where $\lambda \cdot \Delta t$ represent losses toward the substrate

